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(54) Title: METHOD FOR DELIVERING CHEMICALS TO AN OIL OR GAS WELL

(57) Abstract: A method of delivering chemicals to well such as an oil or gas well, the method comprising encapsulating the chemicals in or on a carrier particle such as starch, and delivering the carrier-encapsulated chemical to the well.

METHOD FOR DELIVERING CHEMICALS TO AN OIL OR GAS WELL

1	
2	
3	This invention relates to a method for encapsulating
4	chemicals and particularly to a method for starch
5	and wax encapsulation of aggressive chemicals for
6	applications in the oil industry. The invention
7	relates especially to a method of delivering
8	chemicals to an oil or gas well, in encapsulated
9	form.
10	•
11	Advances in drilling and completion technology have
12	revolutionized new field development and the use of
13	sub-sea wells with long tiebacks is now common. The
14	low temperatures and long fluid transport times
15	under sub-sea conditions often result in a wide
16	variety of production chemistry related problems,
17	including corrosion, scale, wax and asphaltene
18	deposition, hydrate formation, bacterial growth and
19	the transport of viscous fluids including emulsions.
20	The control of these problems is usually achieved by
21	continuous chemical injection at the sub-sea well
22	head along separate, multiple injection lines

2

The installation of multiple chemical injection 1 lines is extremely expensive both for subsea 2 wellhead and continuous downhole injection, 3 especially in deepwater environments. 4 5 A deployment method which allowed a reduction in the 6 number of chemical injection lines required to 7 deliver the cocktail of chemicals required at each 8 wellhead would offer significant cost benefits. 9 10 The deployment of combined chemical treatment 11 12 packages, for example scale and corrosion inhibitors, has been considered as one method of 13 14 reducing the number of chemical injection lines. This has been achieved on a limited commercial basis 15 by blending selected oilfield chemicals together to 16 form a compatible mixture. However, the development 17 of combined chemical packages is fraught with 18 difficulties due to compatibility issues and is 19 limited to a small range of products and product 20 types. This limits the types of combined treatment 21 available and depending upon the nature of the 22 problem often still results in the use of several 23 24 injection lines. 25 26 According to the present invention there is provided 27 a method of delivering a chemical to an oil or gas well, the method comprising associating the chemical 28 29 with a carrier, and delivering the chemical plus carrier to the well. 30 31

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The chemical can be encapsulated by the carrier or 1 otherwise entrapped by the carrier. The carrier 2 preferably comprises a suspension or slurry of 3 particles onto or into which the chemical can be 4 A typical carrier is particulate starch, 5 loaded. but other good carriers can be encapsulating agents 6 conventionally known from e.g. the food, paint and 7 pharmaceutical industries, such as gum arabic, 8 waxes, PVOH, polylactic acids, dextrins, low 9 viscosity modified starches, arabinogalactan, gum 10 acacia, casein, gelatin, carboxymethylcellulose, 11 tragacanth, karaya, sodium alginate, tannin, and 12 13 celluloses. 14 We have found that deploying the chemicals on or in 15 a slurry of nano/micro particles can alleviate 16 compatibility issues during storage and deployment 17 and thus facilitate the injection of multiple 18 chemicals via a single chemical injection line. 19 The nano/micro particles can typically contain a high 20 active level of oilfield chemical, typically 5-21 90%v/v, and can be dispersed in either an aqueous or 22 oleic medium, and in solution or suspension, 23 depending upon the nature of the encapsulation 24 25 The entrapped oilfield chemicals are matrix. typically released upon contact with the produced 26 fluids due to the breakdown of the coating or 27 carrier matrix either thermally and/or as a result 28 of mixing with oil or water. 29 The potential to control the rate and extent of release as a function 30

of time can also allow chemicals to be transported

and released along different sections of the

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31

1	pipeline, thus alleviating some of the kinetic
2	problems associated with scale, wax and hydrate
3	inhibitors in long subsea tie backs.
4	
5	This can enable the simultaneous delivery of
6	combined oilfield chemical packages to platform,
7	remote and complex wells through a single injection
8	line. The oilfield production chemical-entrapped
9	particles could be injected topsides, at sub sea
10	wellheads or elsewhere in the well. The particles
11	could also be applied to deliver oilfield chemicals
12	that cannot be effectively deployed by conventional
13	solvents. Certain embodiments may include the
14	delivery of a single oilfield chemical to a well
15	while associated with a carrier such as the above-
16	mentioned compounds.
17	
18	The chemical is typically injected continuously into
19	the well, typically through a dedicated fluid line.
20	the second secon
21	The nano/micro particle entrapment technology can be
22	applied to deliver a wide range and a wide
23	combination of oilfield production chemicals down
24	one injection line or umbilical. This includes, but
25	is not limited to scale inhibitors, corrosion
26	inhibitors, wax inhibitors, asphaltene inhibitors,
27	hydrate inhibitors, oxygen scavengers, hydrogen
28	sulphide scavengers, demulsifiers, biocides, gel
29	breakers, tracers, friction reducers, surfactants,
30	de-oilers and antifoaming agents. The oilfield
31	chemicals can be entrapped in either liquid or solid
32	form.

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1	The	particles	can be	manufactured	using	a	variety	7 0	£
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- 2 techniques including complex coacervation,
- 3 interfacial polymerisation, desolvation, extrusion,
- 4 agglomeration, emulsion polymerisation, gelation,
- 5 chemical vapour deposition, fluid bed coating, spray
- 6 drying and combinations thereof. The particles can
- 7 be produced over a variable particle size,
- 8 typically, $1nm-850\mu m$ and can contain a high active
- 9 level of oilfield chemical, typically 1-90%v/v.
- 10 Nano/micro particles containing different oilfield
- 11 production chemicals can be dispersed into either an
- 12 aqueous or oleic carrier fluid, that may or may not
- 13 contain other oilfield production chemicals, using
- 14 either ionic or non-ionic surface active agents.
- 15 The material is preferably stable under injection
- 16 conditions in both aqueous and non-aqueous
- 17 environments at the ambient and sub-ambient
- 18 temperatures that may be encountered in a production
- 19 environment. The entrapped oilfield chemical can be
- 20 rapidly released from the encapsulating and/or
- 21 carrier medium as a result of either thermal
- 22 degradation of the matrix and/or dissolution in
- 23 either the oil or water phase, releasing the
- 24 oilfield chemical under wellhead conditions. The
- 25 release time of the chemical upon contact with the
- 26 produced fluids could also be delayed depending upon
- 27 the nature of the entrapment matrix. This can
- 28 allow chemicals to be transported and released along
- 29 different sections of the pipeline, thus enabling
- 30 the release of chemicals in the right place and
- alleviating some of the kinetic problems associated

with scale, wax and hydrate inhibitors in long sub 1 2 sea tie backs. 3 4 The entrapment of certain oilfield chemicals could reduce the corrosivity of the fluid to be deployed 5 into the wellhead or downhole injection system. 6 This could permit the umbilicals and downhole 7 injection lines to be fabricated from lower cost 8 carbon steels rather than the more expensive 9 stainless steels and/or corrosion resistant alloys. 10 11 12 The particles containing different production chemicals, in either solid or liquid form, can then 13 be mixed together to produce the required blend of 14 15 oilfield chemicals for dispersion into the fluid 16 carrying medium which may be aqueous or organic 17 The solid particles could be dispersed into 18 the fluid-carrying medium by use of a wide range of 19 different types of amphoteric, anionic, cationic and 20 nonionic surface-active agents. Amphoteric surfactants could include acetates such as lauro-, 21 alkyl- and coco-amphoacetates, betaines such as 22 lauryl-, alkyl- and coco-amidopropylbetaines, 23 glycinates, imidazolines and propionates such as 24 25 lauro-, alkyl- and coco-aminodipropionate. Anionic surfactants could include alkyl- alkylaryl-, 26 27 alkylether and alkylarylether sulphonates and 28 carbonates, lignin derivatives, olefine and paraffin sulphonates, phosphate esters and sarcosinates. 29 30 Cationic surfactants could include amides, amines, 31 amidoamines, diamines and quaternaries such as

didecyldimethylammonium. Nonionic surfactants could

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include alkoxylates such as alcohol-, alkylphenol-,

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2
       amide-, ester-, fatty acid- and glyceride
       ethoxylates, alkylamides, amine oxides and esters.
  3
  4
       The required dispersing characteristics could be
  5
       achieved for example by varying the ratio of a
  6
       sorbitan ester and a sorbitan ester ethoxylate to
  7
       achieve the desired hydrophilic - lipophilic balance
  8
 9
       (HLB).
 10
 11
       The chemical is typically coated or otherwise
12
      associated with a carrier such as starch, flour or
13
             The starch can decompose at a given
      wax.
14
      temperature releasing the chemical at a second
      location where it is needed.
15
                                     Selection of the
      characteristics of the carrier (e.g. starch) used
16
      allows accurate control over the temperature of
17
      decomposition. Normally the temperature at the
18
      wellhead will be hotter than the surface of the
19
20
             The precise temperature at the wellhead will
      vary from well to well, and typical subsea wellheads
21
      may have an ambient temperature of around 110°C
22
23
      (compared with 20°C at surface).
                                        The starch or wax
24
      coat can typically be designed to decompose when it
      crosses a point on the temperature gradient and so
25
26
      release the chemicals.
                              In particular, wax carriers
      can be designed to degrade or dissolve slowly or
27
      after a set time has elapsed to release the
28
29
      chemicals continuously over a period of time or
      after a set interval e.g. in the production fluids.
30
31
      The starch or wax may be modified to decompose at
      different temperatures as may be necessary for
32
```

1 particularly shallow or particularly deep wells or 2 for any other reason in which the temperature of the wellhead may be different from normal. The starch 3 4 is typically granular starch, and resistant starch 5 made therefrom. The chemical is typically adsorbed onto the starch, typically by simple mixing. 6 7 Adjuncts useful in controlled release formulations can be added. 8 9 10 All granular starches and flours (hereinafter 11 "starch") may be suitable for use herein and may be 12 derived from any native source. A native starch as 13 used herein, is one as it is found in nature. 14 suitable are starches derived from a plant obtained by standard breeding techniques including 15 16 crossbreeding, translocation, inversion, transformation or any other method of gene or 17 chromosome engineering to include variations 18 19 thereof. In addition, starch derived from a plant 20 grown from artificial mutations and variations of 21 the above genetic composition, which may be produced by known standard methods of mutation breeding, are 22 23 also suitable herein. 24 25 Typical sources for the starches are cereals, 26 tubers, roots, legumes and fruits. The native 27 source can be corn, pea, potato, sweet potato, banana, barley, wheat, rice, sago, amaranth, 28 29 tapioca, arrowroot, canna, sorghum, and waxy or high amylose varieties thereof. As used herein, the term 30 "waxy" is intended to include a starch containing at 31 32 least about 95% by weight amylopectin and the term

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"high amylose" is intended to include a starch 1 containing at least about 40% by weight amylose. 2 3 Conversion products which retain their granular 4 structure may be derived from any of the starches, 5 including fluidity or thin-boiling starches prepared 6 by oxidation, enzyme conversion, acid hydrolysis, 7 heat and or acid dextrinization, and or sheared 8 9 products may also be useful herein. 10 Particularly useful are granular structures, which 11 have been "pitted" by the action of enzymes or acid, 12 leaving a still organised structure that creates a 13 microporous starch. The enzymatic or acid hydrolysis 14 of the starch granule is carried out using techniques 15 well known in the art. The amount of enzyme used is 16 dependent upon the enzyme, i.e., type, source and 17 activity, as well as enzyme concentration, substrate 18 concentration, pH, temperature, the presence or 19 absence of inhibitors, and the degree and type of 20 21 modification. Types of modifications are described herein, infra. These parameters may be adjusted to 22 optimise the nature and extent of the "pitting" of 23 the starch granule. 24 25 Another particulate starch useful in the controlled 26 release applications of the present invention is 27 resistant starch. Resistant starch is commonly 28 known as a starch not likely to be adsorbed in the 29 small intestine of a healthy individual. or particulate starches, such as of the RS2-type (a starch granule that resists digestion by pancreatic

30

31

10

1 alpha-amylase) and the RS4-type (a chemically 2 modified starch, such as acetylated, 3 hydroxyalkylated, or cross-linked starch) are particularly suitable. However, resistant starches 4 of the RS3-type (retrograded, non-granular starch 5 6 formed by heat/moisture treatment of starch) are 7 also suitable for the instant invention due to their high level of retrogradation or crystallisation from 8 9 the alignment and association of associated amylose. 10 11 These types of resistant starch are well known in the art and may be exemplified by that disclosed in 12 13 US Patent Nos. US 5,593,503 which describes a method 14 of making a granular resistant starch; US Patent Nos. 5,281,276 and 5,409,542 which describe methods 15 of making resistant starches of the RS3 type; US 16 17 5,855,946 which describes a method of making a resistant starch of the RS4-type; and U.S. 18 19 Application Serial No. 60/157370, which describes 20 the formation of a very highly resistant starch. --The methods for making the resistant starches are 21 22 described in the preceding references, the 23 disclosures of which are incorporated herein by 24 reference. 25 The starch particulate, including granular and 26 27 resistant starches, may be modified by treatment with any reagent or combination of reagents that 28 contribute to the controlled release properties of 29 the starch. 30

	chemical modifications are intended to include
2	crosslinked starches, including crosslinking the
3	particulate starch with reactive polymers.
4	Preferred reactive polymers include starches
5	modified with aldehyde or silanol groups. Other
6	chemical modifications include, without limit,
7	acetylated and organically esterified starches,
8	hydroxyethylated and hydroxypropylated starches,
9	phosphorylated and inorganically esterified
10	starches, cationic, anionic, non-ionic, and
11	zwitterionic starches, and succinate and substituted
12	succinate derivatives of starch.
13	
14	Preferred modified starches are starch acetates
15	having a degree of substitution ("DS") of about up
16	to about 1.5, particularly those disclosed in US
17	5,321,132, thereby improving compatibility with
18	synthetic hydrophobic materials. Such
19	modifications are known in the art, for example in
20	Modified Starches: Properties and Uses, Ed.
21	Wurzburg, CRC Press, Inc., Florida (1986).
22	
23	Other suitable modifications and methods for
24	producing particulate starches are known in the art
25	and disclosed in U.S. Patent No. 4,626,288 which is
26	incorporated herein by reference. In a particularly
27	useful embodiment, the starch is derivatized by
28	reaction with an alkenyl cyclic dicarboxylic acid
29	anhydride by the method disclosed in U.S. Patent
30	Nos. 2,613,206 and 2,661,349, incorporated herein by
31	reference, or propylene oxide, more particularly by
32	reaction with octenylsuccinic anhydride.

Τ.	The encapsulated chemicals can be carried in a
2	liquid-phase inhibitor or other chemical to be
3	delivered to the well that may be incompatible with
4	the encapsulated chemical. All chemicals to be
5	delivered could then be injected through a single
6	umbilical. Two umbilicals could be installed to
7	allow operations to continue in the event of one
8	blocking up. Additionally a third umbilical for
9	methanol could be provided. A total of three
10	umbilicals could therefore provide adequate cover
11	for a well. This represents a significant saving
12	when compared with the prior art, which requires
13	five or six umbilicals for comparable performance.
14	
15	Embodiments of the present invention will now be
16	described by way of example with reference to the
17	following examples.
18	
19	Example 1: Encapsulation of solid material
20	US Patent 4755397 to Eden et al (incorporated herein
21	by reference) describes a process for the starch
22	encapsulation of a solid material, namely, ferric
23	hydroxide, which can be adapted for the
24	encapsulation of oilfield chemicals as follows.
25	
26	The desired oilfield chemical is dissolved in
27	acidified water, dilute sodium hydroxide is added as
28	necessary while stirring to remove from the chemical
29	any trace precipitates. Ammonium sulphate, water and
30	high amylose (70%) cornstarch is added to the
31	chemical slurry to give a slurry of the following
32	composition:

1	Starch 410 grams (19.9%)
2	Ammonium sulphate 610 grams (29.6%)
3	Chemical 41 grams (2.0%)
4	Water 1000 grams (48.5%)
5	This slurry is processed through a jet cooker (Model
6	C-1, National Starch & Chemical Corp) at 150°C. At
. 7	this temperature the high amylose starch cooks,
8	despite the presence of a high level of an
9	inhibiting salt, and forms a uniform dispersion. A
10	ball valve attached to the outlet of the jet cooker
11	can be adjusted so that a pressure drop from maximum
12	cooking temperature and pressure to atmospheric
13	pressure occurs as the starch cook passes through
14	the valve. Upstream the pressure is typically
15	90psig; downstream the pressure is typically Opsig.
16	
17	As the starch passes through the valve and the
18	pressure is reduced to atmospheric, its temperature
19	drops to around 104°C, the boiling point of the salt
20	solution at atmospheric pressure. At this
21	temperature, the starch precipitates essentially
22	instantaneously entrapping the solid oilfield
23	chemical. The product collected at the cooker
24	outlet is typically a slurry of tan particles 5 to 7
25	microns in diameter. The slurry, by volume, is a
26	third salt solution and two thirds precipitated
27	particles. This product is washed free of salt and
28	dried.
29	
30	The dried particles (40% by weight) containing the
31	various oilfield chemicals are then mixed with a
32	synthetic white oil such as Isopar M (52% by weight)

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1 and a polyalkoxylated alkyl phenol based dispersant 2 (5% by weight) using a high shear, UltraTurrax mixer at 5000 rpm for 10 minutes. A clay based thickening 3 agent (3% by weight) is then added to this mix and 4 blended using a high shear, UltraTurrax mixer at 5 6 10,000 rpm. 7 8 This process can be used for the production of encapsulated particles containing a) solid biocides; 9 b) de-oilers; c)demulsifiers; d)scale inhibitors; 10 e) corrosion inhibitors; f) wax inhibitors; and 11 g)asphaltene inhibitors. The chemical-loaded 12 13 particles are mixed in various combinations of 14 chemicals and delivered through a single fluid 15 delivery pipeline to a wellhead, where the temperature of around 110°C breaks down the starch 16 17 particles and releases the chemicals. Optionally a 18 liquid chemical such as a corrosion inhibitor is mixed with the carrier fluid conveying the particles 19 20 to the well. 21 22 Example 2: Encapsulation of an Active Ingredient 23 WO9901214 to Fester et al (incorporated herein by reference) describes a process for the encapsulation 24 25 of an active ingredient, namely, solids and watersoluble fluids. This can be adapted for 26 encapsulation of oilfield chemicals as follows. 27 28 29 Fifteen grams of PN (native potato starch) are added to 100ml water in which 2.5 g Tween 80 is dissolved. 30 31 Four grams TSTP are dissolved in this suspension, 32 followed by the addition of 20 g of salad oil. An

emulsion forms with the aid of an Ultra-Turrax. 1 The o/w emulsion is then emulsified in a second 2 hydrophobic phase, namely 200ml of paraffin oil. 3 top stirrer at a speed of 600 rpm is used for this 4 5 purpose. 6 A solution of 0.65g NaOH in 10ml water is 7 subsequently added to the emulsion with stirring, in 8 9 order to initiate partial gelation and crosslinking. After 30 minutes, the stirrer speed is 10 11 increased to 1000 rpm. After 4 hours the emulsion is 12 broken by addition of acetic acid. 13 The starch particles collected in the water/acetic 14 acid phase. After separation, the particles are 15 washed with de-ionised water and stored. 16 Examination of the dispersed fluid by light 17 microscopy should indicate that the particles are 18 essentially mono dispersed with a size of 25 $\mu \mathrm{m}$ 19 20 containing droplets of oil. 21 This process can be used for the production of 22 encapsulated particles containing solid and/or 23 liquid chemicals, namely, scale and corrosion 24 inhibitors, oxygen and hydrogen sulphide scavengers, 25 demulsifiers, gel breakers, tracers and antifoaming 26 27 However, the process could be applicable to any solid or water-soluble chemicals. As before the 28 29 particulate- entrapped chemicals are mixed in various combinations of chemicals and delivered 30 through a single fluid delivery pipeline to a 31 wellhead, where the temperature of around 110°C 32

1	breaks down the starch particles and re	leases the
2	chemicals. Again the liquid phase of t	he carrier
3	fluid can incorporate a further chemica	l to be
4	delivered to the well.	
5		
6	Example 3: Encapsulation of a Water Ins	oluble Liquid
7	US Patent 4755397 to Eden et al (incorp	orated herein
8	by reference) describes a process for t	he starch
9	encapsulation of a water insoluble liqu	id, namely,
10	peppermint oil, and this can be adapted	for the
11	production of starch encapsulation of h	ydrophobic
12.	oilfield chemicals as follows.	
13		
14	A slurry is made of the following compo	sition:
15	High Amylose (70%Corn Starch) 20%	
16	Ammonium Sulphate 40%	
17	Water 40%	
18		
19	The following is mixed, to disperse the	hydrophobic
20	oilfield chemical and added, with mixing	g, to the
21	previous slurry:	
22		
23	Oilfield chemical	2-10%
24	Surfactants	90-98%
25		
26	The resulting slurry/coarse emulsion is	jet-cooked
27 .	through a C-1 cooker as in Example 1. In	this case,
28	the cooker outlet hose empties below the	surface of
29	a slurry of ammonium sulphate and ice in	saturated
30	ammonium sulphate solution (-8°C.) to co	ndense and
31	trap any free peppermint oil vapours. Th	e resulting
32	product is typically coarse (<20 mesh) 1	ight tan

17

1 powder in salt solution. The powder is recovered by 2 filtration and dried. 3 A 3% weight aqueous solution of HEC is then prepared 4 by slowly adding the powdered HEC to distilled water 5 and gradually increasing the mixing speed over a 6 7 five-minute period. Once a solution is formed a sorbitan ester ethoxylate based dispersant (6% by 8 weight) is added to the aqueous HEC mixture and 9 blended at 2000rpm for five minutes. 10 The dried 11 particles (50% by weight) containing the various oilfield chemicals are then mixed with the aqueous 12 solution of HEC and dispersant using a high shear, 13 UltraTurrax mixer at 5000 rpm for 10 minutes. 14 15 This process is particularly useful for 16 manufacturing encapsulated products containing oil 17 soluble scale and corrosion inhibitors, wax and 18 asphaltene inhibitors, drag reducers, demulsifiers 19 20 and de-oilers. A variety of these chemicals can be encapsulated as described above and delivered to a 21 wellhead via a single injection line in various 22 combinations, without interaction between the 23 chemicals in the line during delivery. Upon arrival 24 at the wellhead the starch capsules surrounding the 25 chemicals are broken down by the ambient temperature 26 at the wellhead, and the chemicals are released and 27 28 activated in situ. Incorporation of incompatible liquid phase chemicals in the carrier fluid does not 29 affect the encapsulated chemical. 30

18

Example 4: Encapsulation of a solid or oil soluble 1 2 product. US Patent 4997659 to Yatka et al (incorporated 3 4 herein by reference) describes a process for the encapsulation of a powdered sweetener, namely, 5 Alitame in paraffin and/or microcrystalline wax. 6 This was adapted for the encapsulation of various 7 solid oilfield chemicals as listed above. 8 9 A 20% paraffin or micro-crystalline wax, of defined 10 melting point/80% solid oilfield chemical is 11 prepared by mixing the molten wax with the solid 12 chemical, cooling to form an agglomerate and 13 grinding up the agglomerate to form granules. 14 granules are optionally further processed to form 15 spheres, using a spheroniser. The size of the 16 spheres is controlled by the granulation process but 17 is typically 1-50 μ m in diameter. 18 19 This process is typically used to produce paraffin 20 or microcrystalline wax-based particles containing 21 solid oilfield production chemicals such as scale, 22 23 wax and corrosion inhibitors, biocides and other scavengers. In addition the wax particles can be 24 25 manufactured to entrap oil-based liquids such as 26 corrosion, wax and asphaltene inhibitors, 27 demulsifiers and de-oilers. 28 29 The nano/micro particles containing different production chemicals, in either solid or liquid 30 form, are dispersed together to produce the required 31 32 blend of oilfield chemicals for dispersion into the

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7	fluid carrying medium which was either aqueous or
2	organic based. The solid particles are dispersed
3	into the fluid-carrying medium by use of a wide
4	range of different dispersants. Suitable
5	dispersants include fatty acid esters and
6	alkoxylated (e.g. methoxylated or ethoxylated) fatty
7	acid esters such as sorbitan ester and sorbitan
8	ester ethoxylate; and PEG esters such as PEG
9	laurate. By varying the ratio of the ethoxylated
10	sorbitan ester to the sorbitan ester the desired HLB
11	can be obtained.
12	
13	The encapsulated oil field chemicals are mixed in
14	the desired proportions and delivered via a single
15	fluid delivery line to a wellhead, at which point
16	the wax capsules degrade, releasing the chemical
17	into the wellhead environment. Optionally the two
18	or more chemicals that are delivered to the well can
19	be encapsulated by different methods e.g. according
20	to any of the examples herein, so that the different
21	particles release their chemical burdens at
22	different points in the well, in response to
23	different stimuli.
24	
25	Example 5: Encapsulation of a wax inhibitor by
26	starch.
27	A granular starch (150g, starch octenylsuccinate,
28	aluminum salt, commercially available from National
29	Starch and Chemical Company) was added to a wax
30	inhibitor XPC 3147C (50 g, Aldrich) which had been
31	melted at a temperature greater than 30°C. The
32	mixture was stirred at ambient temperature and

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20

1 pressure in a high shear disperser (Torrence, #785049) at 2000-4000 rpm. An additional 100 g of 2 3 the granular starch was added to the mixture and stirred for two more minutes to form a fine, free-4 5 flowing powder. This is conveyed to a wellhead as previously described through a single fluid line by 6 7 a carrier fluid that incorporates a scale inhibitor that is incompatible with the wax inhibitor, without 8 any reaction between the chemicals. 9 The scale inhibitor treats the fluid conduit continuously from 10 the point of entry to the wellhead, and the wax 11 inhibitor is activated only after a longer period of 12 13 time as a result of the starch encapsulating matrix 14 dissolving in the produced fluids. 15 Example 6: Encapsulation of a water-soluble chemical 16 17 by starch. Water-soluble solids were formulated with starch at 18 19 a 1:1 ratio (50% loading on starch). The oil well chemical was solubilised in ambient water and 20 21 homogenised for 1-2 minutes at 9000-10000 rpm 22 (Silverson L4RT). The starch was then added to the solution and the mixture was further homogenised for 23 24 2-3 minutes at 9000-10000rpm, 20°C (Silverson L4RT). 25 The mixture was spray dried (40% solids, 375°F inlet 26 temperature, 225°F outlet temperature with a feed 27 rate of 160ml/minutes and dual wheel atomisation using Bowen Lab Model (30" x 36") to produce a 28

29 30

31 a. The example was carried out using a scale 32 inhibitor, Scaletreat 2001-28, as the oil well

flowable, non-sticky composition.

1	chemical and Vulca 90, a maize starch
2	crosslinked with 1.5% epichlorohydrin on dry
3	starch.
4	b. The example was carried out using a corrosion
5	inhibitor, Corrtreat 2001-29 as the oil well
6	chemical and a starch acetate (1.5 DS) waxy
7	maize starch.
8	c. The example was carried out using a scale
9	inhibitor, Scaletreat 2001-26 as the oil well
10	chemical and a microporous waxy maize starch
11	that was digested using 0.3% glucoamylase on
12	dry starch to achieve 15% digestion.
13	
14	In each case, the encapsulated chemicals are mixed
15	as desired and delivered in mixtures of encapsulated
16	particles to the well-head through a single fluid
17	line. The encapsulated particles are degraded by
18	the fluid conditions at the well-head, and/or by
19	temperature, thereby delivering their active
20	reagents at the required position in the wellhead.
21	
22	Example 7: Encapsulation of a water insoluble
23	chemical by starch.
24	Water insoluble solids were formulated with starch
25	at a 1:1 ratio (50% loading on starch). The oil
26	well chemical was added to a waxy maize starch
27	modified with 3% octenyl succinic anhydride and
28	converted to a water fluidity of 40, and the mixture
29	was homogenised for 1-2 minutes at 9000-10000 rpm,
30	20°C (Silverson L4RT). Water was added to the
31	emulsion and the mixture was further homogenised, 1
32	minute at 9000-10000 rpm, 20°C (Silverson L4RT).

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1 The starch was then added to the solution and the

22

- 2 mixture was further homogenised, 1-2 minutes at
- 3 9000-10000 rpm, 20°C (Silverson L4RT). The mixture
- 4 was spray dried (35% solids, 380°F inlet
- 5 temperature, 230°F outlet temperature, 140-
- 6 160ml/minutes with dual wheel atomisation using
- 7 Bowen Lab Model (30" x 36")) to produce a flowable,
- 8 non-sticky composition.

- 10 a. The example was carried out using a wax
- inhibitor, Waxtreat 398 as the oil well chemical
- and a microporous waxy maize which was 30%
- digested with 0.3% glucoamylase, and modified
- 14 with 3% octenyl succinic anhydride and
- 15 crosslinked with 1% aluminium sulphate.
- b. The example was carried out using an asphaltene
- 17 dispersant, Waxtreat 7302 as the oil well
- chemical and a microporous waxy maize starch
- 19 modified using 3% octenyl succinic anhydride,
- enzymatically treated using 0.3% glucoamylase, to
- 21 achieve 30% digestion.
- 22 c. The example was carried out using a hydrogen
- sulphide scavenger, Scavtreat 1020 as the oil
- 24 well chemical and a high amylose corn starch,
- 25 HYLON® VII starch, commercially available from
- 26 National Starch and Chemical Company.
- 27 d. The example was carried out using a kinetic
- 28 hydrate inhibitor, Hytreat 569 as the oil well
- chemical and a microporous (30% enzyme digested)
- 30 waxy maize starch modified using 3% octenyl
- 31 succinic anhydride, enzymatically treated using
- 32 0.3% glucoamylase.

1 e. The example was carried out using an antiagglomerate hydrate inhibitor, Hytreat A560 as 2 the oil well chemical and a cationic starch 3 4 silanol, 0.3% Nitrogen, 0.4% silanol. 5 Chemicals are delivered through a single delivery 6 line to a wellhead and also to a well bore and 7 The wellhead chemicals are released from 8 formation. their encapsulated particles at the prevailing 9 wellhead conditions and the formation chemicals are 10 only released upon reaching the more aggressive 11 prevailing conditions at the formation. 12 13 14 Example 8 Starch was weighed out into a glass container. 15 The oil well chemical was added while mixing for 5 16 minutes and then mixed for an additional 5 minutes, 17 or until uniform using a Powerstat, Variable 18 Autotransformer set at 80 (3PN168), Bodine Electric 19 Co, Speed reducer motor (NSE-12R). 20 21 a. Starch used was a 50:50 blend of sago and 22 23 tapioca, DD and the oil well chemical used was 24 Waxtreat 398. The starch: chemical ratio used was 25 100:40 and the loading was 28.6%. b. Starch used was a high amylose (70%) maize starch 26 modified by 3% octenyl succinic anhydride and 10% 27 polyvinyl alcohol and the oil well chemical used 28 29 was Waxtreat 398. The starch: chemical ratio used 30 was 100:80 and the loading was 44.4%.

c. Starch used was enzyme converted (alpha amylase)

maltodextrin and the oil well chemical used was

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24

1	Trosquat. The starch:chemical ratio used was
2	100:38 and the loading was 27.5%.
3	d. Starch used was enzyme converted (alpha amylase)
4	maltodextrin and the oil well chemical used was
5	Trosquat. The starch:chemical ratio used was
6	100:38 and the loading was 27.5%.
7	e. Starch used was a high amylose (70%) maize that
8	was gelatinised, completely enzymatically de-
9	branched and retrograded and the oil well
10	chemical used was Hytreat A560. The
11	starch:chemical ratio used was 100:24 and the
12	loading was 19.3%.
13	
14	The encapsulated chemicals are mixed as desired and
15	delivered to production tubing or other well
16	tubulars through a single fluid line. Once reaching
17	the target in the well the chemicals are released
17	the target in the well the chemicals are released
17 18	the target in the well the chemicals are released
17 18 19	the target in the well the chemicals are released through reaction to local conditions.
17 18 19 20	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the
17 18 19 20 21	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any
17 18 19 20 21	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be
17 18 19 20 21 22	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any
17 18 19 20 21 22 23	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any way limited to the delivery of chemicals to the
17 18 19 20 21 22 23 24	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any way limited to the delivery of chemicals to the wellhead, and in certain embodiments the delivery
17 18 19 20 21 22 23 24 25 26	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any way limited to the delivery of chemicals to the wellhead, and in certain embodiments the delivery target is another portion of the well, such as the
17 18 19 20 21 22 23 24 25 26 27	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any way limited to the delivery of chemicals to the wellhead, and in certain embodiments the delivery target is another portion of the well, such as the formation, the reservoir, the casing, production
17 18 19 20 21 22 23 24 25 26 27 28	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any way limited to the delivery of chemicals to the wellhead, and in certain embodiments the delivery target is another portion of the well, such as the formation, the reservoir, the casing, production
17 18 19 20 21 22 23 24 25 26 27 28	the target in the well the chemicals are released through reaction to local conditions. The wellhead is the preferred target of the chemicals delivered in order to protect the tie backs etc from corrosion or blockage, but it will be appreciated that the present invention is not in any way limited to the delivery of chemicals to the wellhead, and in certain embodiments the delivery target is another portion of the well, such as the formation, the reservoir, the casing, production tubing or other tubular or conduit.

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1	through a single injection line. Some embodiments
2	also facilitate the deployment of certain chemicals
3	that are difficult to handle, for example, because
4	they are very corrosive and/or are insoluble in
5	conventional solvents; for example, polyacrylate wax
6	inhibitors, either alone or in combination with
7	other chemicals, where the chemicals or at least one
8	of them cannot be effectively deployed by
9	conventional solvents.
10	
11	Certain embodiments also enable the deployment of
12	oilfield chemicals at high active concentrations,
13	for example, ethylene vinyl acetate (EVA) wax
14	inhibitors that cannot be effectively deployed at
15	>10%v/v by conventional solvents.
16	
17	While starch is a preferred entrapping or coating
18	medium a range of other materials could be used such
19	as natural gums, cellulose and derivatives,
20	polysaccharides, gelatin, wax, fatty acids, acrylic,
21	carboxyvinyl polymers, polyester, polystyrene,
22	polycaprolactone, polyvinyl acetate, polyamides,
23	polyvinyl alcohol, polylactic acid, polyglycolide,
24	shellac, zein, oil based gels, silica gel and other
25	materials consisting of mixtures, copolymers,
26	terpolymers and hydrophobically and/or
27	hydrophilically modified and cross-linked
28	derivatives of the above.
29	
30	In certain embodiments the nano/micro particles can
31	be dispersed in an aqueous or oleic medium depending
32	upon the encapsulation matrix, and can contain one

26

or more soluble or dispersed oilfield production	1	or	more	soluble	or	dispersed	oilfield	production
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2 chemicals.

3

4 Modifications and improvements can be incorporated

5 without departing from the scope of the invention.

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1	Cla	ims
2	1.	A method of delivering a chemical to an oil or
3		gas well, the method comprising associating the
4		chemical with a carrier, and delivering the
5		chemical and carrier to the well.
6		
7	2.	A method as claimed in claim 1, wherein the
8		chemical is encapsulated by the carrier.
9		
10	3.	A method as claimed in any preceding claim,
11		wherein the chemicals are released from the
12		carrier upon contact with the produced fluids
13		in the well.
14		
15	4.	A method as claimed in any preceding claim,
16		wherein two or more chemicals are delivered via
17		a single chemical injection conduit.
18		
19	5.	A method as claimed in claim 4, wherein the two
20		chemicals are mutually incompatible.
21		
22	6.	A method as claimed in claim 4 or claim 5,
23		wherein the two or more chemicals are released
24		from the carrier at different locations in the
25		well.
26		
27	7.	A method as claimed in any preceding claim,
28		wherein the or each chemical is aggressive,
29		insoluble or corrosive.
30		

1	8.	A method as claimed in any preceding claim,
2		wherein the chemical and carrier are carried by
3		a fluid to the desired point of delivery.
4		•
5	9.	A method as claimed in claim 8, wherein the
6		fluid phase carries a further chemical to be
7		delivered to the well.
8		
9	10.	A method as claimed in claim 8 or claim 9,
10		wherein the fluid is aqueous fluid.
11		
12	11.	A method as claimed in claim 8, or claim 9
13		wherein the fluid is oleic or organic fluid.
14		
15	12.	A method as claimed in any preceding claim,
16		wherein the chemical-bearing carrier is
17		injected at surface.
18		
19	13.	A method as claimed in any preceding claim,
20		wherein the chemical-bearing carrier is
21		injected at a wellhead.
22		·
23	14.	A method as claimed in any preceding claim,
24		wherein the chemical is selected from the group
25		comprising scale inhibitors, corrosion
26		inhibitors, wax inhibitors and dispersants,
27		asphaltene inhibitors and dispersants, hydrate
28		inhibitors, oxygen scavengers, pour-point
29		modifiers, hydrogen sulphide scavengers,
30		demulsifiers, biocides, gel breakers, tracers,
31		friction reducers, surfactants, de-oilers and
32		antifoaming agents.

1	15.	A method as claimed in any preceding claim,
2		wherein the carrier is associated with the
3		chemical by a technique selected from the group
4		comprising coacervation, interfacial
5		polymerisation, desolvation, extrusion,
6		agglomeration, emulsion polymerisation,
7		gelation, chemical vapour deposition, fluid bed
8		coating, spray drying and combinations thereof.
9		
10	16.	A method as claimed in any preceding claim,
11		wherein the carrier is selected from the group
12		comprising starch or flour, gum arabic, waxes,
13		PVOH, polylactic acids, dextrins, low viscosity
14		modified starches, arabinogalactan, gum acacia,
15		casein, gelatin, carboxymethylcellulose,
16		tragacanth, karaya, sodium alginate, tannin,
17		and celluloses.
18		
19	17.	A method as claimed in any preceding claim,
20		wherein the chemical is continuously delivered
21		to the well.
22		
23	18.	A method as claimed in any preceding claim,
24		wherein the carrier and chemical forms a
25		particle.
26		
27	19.	A method as claimed in claim 18, wherein the
28		particle size is in the range of 1µm-20µm.
29		
30	20.	A method as claimed in any preceding claim,
31		wherein the carrier dissolves into the produced

- fluids from the well after releasing the
- 2 chemical.

INTERNATIONAL SEARCH REPORT

Inten I Application No PCT/GB 01/03547

CLASSIFICATION OF SUBJECT MATTER C 7 E21B37/06 E21B E21B43/25 According to International Patent Classification (IPC) or to both national classification and IPC B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) IPC 7 E21B Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Electronic data base consulted during the international search (name of data base and, where practical, search terms used) EPO-Internal C. DOCUMENTS CONSIDERED TO BE RELEVANT Category * Citation of document, with indication, where appropriate, of the relevant passages Relevant to claim No. X US 4 611 664 A (OSTERHOUDT III M GLENN ET 1-3,13,AL) 16 September 1986 (1986-09-16) column 2, line 35 -column 3, line 13; claims 1,2,5-9,12-16 column 4, line 21 - line 49 US 4 986 354 A (CANTU LISA A ET AL) X 1-3,8, 22 January 1991 (1991-01-22) 10-12. 14,15, 17-20 column 1, line 38 -column 4, line 2 X Further documents are listed in the continuation of box C. X Patent family members are listed in annex. Special categories of cited documents : "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international "X" document of particular relevance; the claimed Invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone filling date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "Y" document of particular relevance; the claimed invention cannot be considered to involve an invention step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. "O" document referring to an oral disclosure, use, exhibition or other means *P* document published prior to the international filing date but later than the priority date claimed *&* document member of the same patent family Date of the actual completion of the international search Date of mailing of the international search report 4 December 2001 12/12/2001 Name and mailing address of the ISA **Authorized officer** European Patent Office, P.B. 5818 Patentham 2 NL - 2280 HV Rijswijk Tel (+31-70) 340-2040, Tx. 31 651 epo ni, Fax: (+31-70) 340-3016 Boulon, A

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INTERNATIONAL SEARCH REPORT

Interna Application No
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